Cost Analysis of K-Out of-n Repairable System with Dependent Failure and Stand by Support Using Kolmogorov's Forward Equations Method

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Abstract: Problem statement: Many authors have studied k-out of-n repairable system with dependent failure and standby support. The question was raised whether the repair and standby units support increase the reliability of the system. Determine the efficiency of repair and standby support on the reliability of the system. **Approach:** In this study the statistical analysis of k-out of-n repairable system with dependent failure and standby support were discussed. Several reliability characteristics are obtained by using Kolmogorov's forward equations method. After the model is developed a particular case study is discussed to validate the theoretical results, a numerical computation are derived. Tables and graphs have been also given in the end. **Results:** The results indicated that the system with repair and standby support is better than the system without repair and standby support. **Conclusion:** These results indicated that the system.

Key words: Cost analysis, Mean Time to System Failure (MTSF), steady-state availability, busy period, profit function, preventive maintenance, Kolmogorov's forward equations method

INTRODUCTION

When a system is constructed, it is assumed that the failure of any unit in k-out of-n systems does not affect the functioning of the system. Nevertheless, in practice, the failure of any working unit of a system results in the reduction of the efficiency of the whole system. It increases stress on the others ones and as the result, the failure rate of functional ones increased and the reliability of the system reduced. Thus, dependence occurs and as a result the failure rates of the units degrade.

The system with standby redundancy facility has been studied for many different system structures. In a redundant system, some additional parts are connected to the system. On the failure of the operating unit, a standby unit is switched on by perfect switching device. The redundancy in a system is usually employed to design highly reliable systems. Also the repairing failed component increases the reliability of the system. If resources are allocated to repair failed components, we should be able to keep for a much longer time. Thus introducing redundant parts and repairing a failed units may achieve high degree of reliability.

Many authors have discussed k-out of-n system with dependent failure rates^[1,2]. The system reliability of modeling shared load was investigated by Shao and Lamberson *et al.*^[3]. Moustafa^[4] studied a transient analysis of reliability with and without repair for k-out

of-n G systems. Pham^[5] studied availability and Mean Life Time of degraded system with partial repair. Who Kee Chang^[6], studied reliability analysis of a repairable parallel system with standby involving human and common-cause failure. Madhu Jain *et al.*^[7] studied k-out of-n repairable system with dependent failure and standby support, but they didn't consider the cost analysis of the system.

The purpose of this study is to discuss cost analysis of k-out 0f-n: G system with active standby redundancy components and repair facility. The system is failed if (k+1) of its n components are failed. If resources are allocated to repair failed components, we should be able to keep the number of failed components below n+s-k+1 for a much longer time. The failure and repair rate times follow exponential distribution. We analyze the system by using Kolmogorov's forward equations. Initially one unit is operative and the other is kept as cold standby. A particular case when no repair and standby support have been discussed. Tables and graphs have been also given in the end.

System description:

- The system consists of a main unit, n-subsystem and s-standbys
- The entire system is working if at least k of its n subsystems are operating

- The system is failed when the number of working components goes down below k
- All active components are follow exponential distribution
- The system is failed when the number of working components goes down below k or the number of failed components has reached n+s-k+1
- The failure and repair rate times follow exponential distribution
- The failure of main unit, which supervises the system, causes the total system failure and has a constant failure rate λ_p
- The failure of fault coverage is constant and equal to $\lambda_{\rm c}$
- The failure rates of all subsystems are constant and same and depend on the number of working units and equal to λ_i, (j = 1, 2,n)
- When any of the operating subsystem fails, it is replaced by standby unit and failed unit goes to repair mode with rate μ_i. The standby units have constant failure rates β
- If all the standbys are consumed, the system works as degraded system until k-subsystems works
- When the system is down, no farther units can failed
- The state of the system is defined to be the number of failed components

The system state transition diagram is given in Fig. 1. State i indicating that exactly i subsystems are failed at time 't', (i = 1, 2,...., n + s - k). The failure rate from state i to state i+1 given by Δ_i . The state transition rate of the system is given by:

$$\Delta_{i} = \begin{cases} n\lambda_{n} - (s-i)\beta & 0 \le i \le s\\ (n+s-i)\lambda_{n+s-i} & s+1 \le i \le n+s-k \end{cases}$$
(1)

The following system characteristics are obtained:

- Mean time to system failure (MTTF) with and without repair
- Steady state availability with and without repair
- Profit function

Formulation of mathematical model: If we let P (t) denote the probability row vector at time t, the initial conditions for this problem are:

$$P_0(0) = 1, P_i(0) = 0, i = 1, 2, \dots, n + s - k + 1$$

By employing the method of linear first order differential equations For Fig. 1 and, we can obtain the following differential equations:

$$P'_{0}(t) = -(\lambda_{0} + \lambda_{p} + \lambda_{c})P_{0}(t) + \mu_{1}P_{1}(t)$$
(2a)

$$P'_{0}(t) = -(\Delta_{i} + \lambda_{p} + \mu_{i})P_{i}(t) + \Delta_{i-1}P_{i-1}(t) + \mu_{i+1}P_{i+1}(t),$$

$$1 \le i \le n + s - k$$
(2b)

$$P'_{n+s-k+1}(t) = -(\mu_{n+s-k+1})P_{n+s-k+1}(t) + \Delta_{n+s-k}P_{n+s-k}(t)$$
(2c)

Where:

$$\begin{split} \Delta_0 &= 4(\lambda_4) + 2\beta, \\ \Delta_1 &= 4(\lambda_4) + \beta, \\ \Delta_2 &= 4\lambda_4, \\ \Delta_3 &= 3\lambda_3 \end{split}$$

This can be written in the matrix form:

$$P^* = QP$$

Where:

$$\mathbf{P}^{*} = \begin{bmatrix} \mathbf{P}_{0}'(t) \\ \mathbf{P}_{1}'(t) \\ \vdots \\ \vdots \\ \mathbf{P}^{*}_{n+s-k}(t) \\ \mathbf{P}^{*}_{n+s-k+1}(t) \end{bmatrix}, \mathbf{P} = \begin{bmatrix} \mathbf{P}_{0}(t) \\ \mathbf{P}_{1}(t) \\ \vdots \\ \mathbf{P}_{0}'_{n+s-k+1}(t) \\ \mathbf{P}^{*}_{n+s-k+1}(t) \end{bmatrix}$$

$$Q = \begin{bmatrix} -(\Delta_0 + \lambda_p + \lambda_c) & \mu_1 & 0 & 0 & \cdots & 0 & 0 & 0 \\ \Delta_0 & -(\Delta_1 + \lambda_p + \mu_1) & \mu_2 & 0 & \cdots & 0 & 0 & 0 \\ 0 & \Delta_1 & -(\Delta_2 + \lambda_p + \mu_2) & \mu_3 & \cdots & 0 & 0 & 0 \\ \vdots & \vdots & \Delta_2 & -(\Delta_3 + \lambda_p + \mu_3) & \cdots & \vdots & \vdots & 0 \\ \vdots & \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & 0 \\ \vdots & \vdots & \vdots & \vdots & \cdots & \vdots & \vdots & 0 \\ \vdots & \vdots & \vdots & \vdots & \cdots & \vdots & \vdots & 0 \\ 0 & 0 & 0 & 0 & \cdots & 0 & \Delta_{n+s-k} + \lambda_p + \mu_{n+s-k}) & \mu_{n+s-k+1} \\ 0 & 0 & 0 & 0 & \cdots & 0 & \Delta_{n+s-k} & -(\mu_{n+s-k+1}) \end{bmatrix}$$



Fig. 1: State transition diagram

Particular case: If we put n = 4, k = 3, s = 2, in equations (3-1) - (3-3), we obtain the matrix form:

 $P^* = QP$

Where: $P_{0}'(t)$ $P_{1}'(t)$ $P^* = |P_2'(t)|$ $P_{3}'(t)$ $P_{4}'(t)$ $P_0(t)$ $P_{1}(t)$ $P = | P_1(t) |$ $P_{1}(t)$ $P_{1}(t)$ 0 0 0 μ_2 0 0 $-(\Delta_2 + \lambda_p + \mu_2) \qquad \mu_3$ 0 $\begin{array}{cccc} -(\Delta_{2} + \lambda_{p} + \mu_{2}) & \mu_{3} & 0 \\ \Delta_{2} & -(\Delta_{3} + \lambda_{p} + \mu_{3}) & \mu_{4} \\ 0 & \Delta_{3} & -\mu_{4} \\ -(\Delta_{0} + \lambda_{p} + \lambda_{c}) & \mu_{1} \\ \Delta_{0} & -(\Delta_{1} + \lambda_{p} + \mu_{i}) \\ 0 & \Delta_{1} \end{array}$ Q =

Mean Time to System Failure (MTSF): Using the above-mentioned set of assumptions and method of linear first order differential equations, the mean time to system failure (MTSF) for the proposed system can be evaluated. To calculate the MTSF we take the transpose matrix of Q and delete the rows and columns

for the absorbing state, the new matrix is called A. the expected time to reach an absorbing state is calculated from:

$$MTSF = P(0)(-A^{-1}) \begin{bmatrix} 1\\1\\1\\1\\1 \end{bmatrix}$$
(3a)
$$Q = \begin{bmatrix} -(\Delta_0 + \lambda_p + \lambda_c) & \Delta_0 & 0\\ \mu_1 & -(\Delta_1 + \lambda_p + \mu_1) & \Delta_1\\ 0 & \mu_2 & -(\Delta_2 + \lambda_p + \mu_2)\\ 0 & 0 & \mu_3\\ 0 & 0\\ 0 & 0\\ -(\Delta_2 + \lambda_p + \mu_3) \end{bmatrix}$$

$$MTTF = \frac{(a_1 + a_2 + a_3)}{a_4}$$
(3b)

$$\begin{split} & \text{Where:} \\ a_1 &= ((\Delta_1 + \mu_1 + \lambda_p)((\Delta_2 + \mu_2 + \lambda_- \{p\})(\Delta_3 + \mu_3 + \lambda_p) - \Delta_2 \mu_3) - \\ & \Delta_1 \mu_2(\Delta_3 + \mu_3 + \lambda_p)) \\ a_2 &= \Delta_0((\Delta_2 + \mu_2 + \lambda_p)(\Delta_3 + \mu_3 + \lambda_p) - \Delta_2 \mu_3) \\ a_3 &= \Delta_0 \Delta_1((\Delta_3 + \mu_3 + \lambda_p) + \Delta_2) \\ a_4 &= (\Delta_0 + \lambda_p + \lambda_c)((\Delta_1 + \mu_1 + \lambda_p)((\Delta_2 + \mu_2 + \lambda_p)(\Delta_3 + \mu_3 + \lambda_p) - \\ & \Delta_2 \mu_3) - \Delta_1 \mu_2(\Delta_3 + \mu_3 + \lambda_p)) - \Delta_0 \mu_1((\Delta_2 + \mu_2 + \lambda_p)(\Delta_3 + \mu_3 + \lambda_p) - \\ & \lambda_p) - \Delta_2 \mu_3 \end{split}$$

When repair is not available, the Mean Time to System Failure (MTTF) is given by:

MTTF =
$$\frac{(b_1 + b_2 + b_3)}{b_4}$$
 (3c)

$$\begin{split} & \text{Where:} \\ & b_1 = (\Delta_1 + \lambda_p)(\Delta_2 + \lambda_p)(\Delta_3 + \lambda_p) \\ & b_2 = (\Delta_2 + \lambda_p)(\Delta_3 + \lambda_p)\Delta_0 \\ & b_3 = \Delta_0 \Delta_1 (\Delta_2 + \Delta_3 + \lambda_p) \\ & b_4 = (\Delta_0 + \lambda_p + \lambda_c)(\Delta_1 + \lambda_p)(\Delta_2 + \lambda_p)(\Delta_3 + \lambda_p) \end{split}$$

Availability analysis: The initial conditions for this problem are the same as for the reliability case:

$$P(0) = [1, 0, 0, 0, 0,]$$

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(4a)

(4c)

the differential equations form can be expressed as:

\mathbf{P}_{0}^{*}		$-(\Delta_0 + \lambda_p + \lambda_c)$	μ_1	0	0	0	P ₀	
P_1^{\ast}		Δ_0	$-(\Delta_1 + \lambda_p + \mu_i)$	μ_2	0	0	P ₁	
P_2^{\ast}	=	0	Δ_1	$-(\Delta_2 + \lambda_p + \mu_2)$	μ_3	0	P ₂	
P_3^*		0	0	Δ_2	$-(\Delta_3 + \lambda_p + \mu_3)$	μ_4	P ₃	
P_4^*		0	0	0	Δ_3	$-\mu_4$	P_4	

In the steady state, the derivatives of the state probabilities become zero, i.e.:

$$QP(\infty) = 0$$

Then the steady state probabilities can be calculated as follows:

$$A(\infty) = P_0(\infty) + P_1(\infty) + P_2(\infty) + P_4(\infty)$$
(4b)

Then the matrix form became:

$$\begin{bmatrix} -(\Delta_{0} + \lambda_{p} + \lambda_{c}) & \mu_{1} & 0 & 0 & 0 \\ \Delta_{0} & -(\Delta_{1} + \lambda_{p} + \mu_{i}) & \mu_{2} & 0 & 0 \\ 0 & \Delta_{1} & -(\Delta_{2} + \lambda_{p} + \mu_{2}) & \mu_{3} & 0 \\ 0 & 0 & \Delta_{2} & -(\Delta_{3} + \lambda_{p} + \mu_{3}) & \mu_{4} \\ 0 & 0 & 0 & \Delta_{3} & -\mu_{4} \end{bmatrix} \begin{bmatrix} P_{0}^{*} \\ P_{1}^{*} \\ P_{2}^{*} \\ P_{3}^{*} \\ P_{4}^{*} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

To obtain $P_0(\infty) + P_1(\infty) + P_2(\infty) + P_4(\infty)$ we solve the Eq. 3a by using following normalizing condition:

 $P_0(\infty) + P_1(\infty) + P_2(\infty) + P_3(\infty) + P_4(\infty) = 1$

We substitute the Eq. 3c in any one of the redundant rows in equation to (3a) yield:

$$\begin{bmatrix} -(\Delta_0 + \lambda_p + \lambda_c) & \mu_1 & 0 & 0 & 0 \\ \Delta_0 & -(\Delta_1 + \lambda_p + \mu_1) & \mu_2 & 0 & 0 \\ 0 & \Delta_1 & -(\Delta_2 + \lambda_p + \mu_2) & \mu_3 & 0 \\ 0 & 0 & \Delta_2 & -(\Delta_3 + \lambda_p + \mu_3) & \mu_4 \\ 1 & 1 & 1 & 1 & 1 \end{bmatrix} \begin{bmatrix} P_0^* \\ P_1^* \\ P_2^* \\ P_3^* \\ P_4^* \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

The steady state availability $A(\infty)$ is given by:

$$A(\infty) = \frac{N}{D}$$
(4d)

Where:

$$N = B_0 B_1 B_2 \mu_4 + \mu_3 \mu_4 (B_0 (B_1 + \mu_2) - \mu_1 (\Delta_0 + \mu_2)) - \mu_4 (\Delta_1 \mu_2 B_0 + \Delta_0 \mu_1 B_2)$$

 $D = B_0 B_1 (B_2 (B_3 + \mu_4) - \Delta_2 \mu_3 + \mu_3 \mu_4) + \mu_4 \mu_3 \mu_2 (B_0 + \mu_1) + \mu_3 \mu_1 \Delta_0 (\Delta_2 - \mu_4) - (B_3 + \mu_4) (\Delta_1 \mu_2 B_0 + \Delta_0 \mu_1 B_2)$

Where:

$$\begin{split} B_0 &= (\Delta_0 + \lambda_p + \lambda_c) \\ B_1 &= (\Delta_1 + \lambda_p + \mu_1) \\ B_2 &= (\Delta_2 + \lambda_p + \mu_2) \\ B_3 &= (\Delta_3 + \lambda_p + \mu_3) \end{split}$$

When there is no repair, the steady state availability of the system is given by:

$$A(\infty) = 0$$

Busy period analysis: The initial conditions for this problem are the same as for the reliability case: the differential equations form can be expressed as availability case.

Then the steady state busy period $B(\infty)$ is given by:

$$\underset{\cdots}{B(\infty)} = 1 - P_0(\infty) = 1 - \frac{\mu_1 \mu_2 \mu_3 \mu_4}{D}$$
(4e)

When there is no repair, the steady state busy period of the system is given by:

 $B(\infty) = 0$

Cost analysis: The expected total profit per unit time incurred to the system in the steady-state is given by:

Profit = total revenue - total cost

$$PF = RA(\infty) - CB(\infty)$$

When there is no repair, the steady state profit of the system is given by:

$$PF = 0$$

Where:

PF = The profit incurred to the system

R = The revenue per unit up-time of the system,

 C_1 = The cost per unit time which the system is under repair>

MATERIALS AND METHODS

Many authors have studied k-out of-n repairable system with dependent failure and standby support. The question was raised whether the repair and standby units support increase the reliability of the system. In this study the statistical analysis of k-out of-n repairable system with dependent failure and standby support were discussed to show the system with repair and standby support increase the reliability of the system.

We analyze the system by using Kolmogorov's forward equations method. After the model is developed a particular case study is discussed to validate the theoretical results. Next, some numerical computations are derived to show the effect of repair and standby support on the system.

RESULTS

If we put: $\lambda_p = 0.002$, $\lambda_c = 0.003$, $\lambda_\beta = 0.005$, $\lambda_4 = 0.01$, $\lambda_3 = 0.03$, $\mu_1 = 0.1$, $\mu_2 = 0.2$, $\mu_3 = 0.3$, $\mu_4 = 0.4$ in Eq. 4b and c; 5d and e we get: $\Delta_0 = 0.05$, $\Delta_1 = 0.045$, $\Delta_2 = 0.04$, $\Delta_3 = 0.09$ and obtain the Table 1-4:

- Table 1 show relation between failure rate λ_p and MTSF of the system (with repair and standby and with repair and without standby and without repair and standby)
- Table 2 show relation between failure rate λ_p and steady state availability of the system (with repair and standby and with repair and without standby)
- Table 3 show relation between failure rate λ_p and busy period of the system (with repair and standby and with repair and without standby)

Table 1: Relation between failure rate λ_p and the MTSF (with and without standby)

	MTTF of the	MTTF of the	MTTF of the
	system	system	system
	with repair	with repair and	without repair
$\lambda_{\rm p}$	and standby	without standby	and standby
0.001	287.90	285.41	70.451
0.002	223.53	221.98	67.259
0.003	182.68	181.62	64.297
0.004	154.45	153.68	61.545
0.005	133.78	133.19	58.984
0.006	117.99	117.52	56.595
0.007	105.53	105.15	54.363
0.008	95.456	95.132	52.276
0.009	87.135	86.859	50.320
0.010	80.148	79.910	48.485

Table 2: 1	Rela	tio	n b	etween	failure rate	λ_p	and	stead	y state	availabilit	y

λ_{p}	Availability of the system with repair and standby	Availability of the system with repair and without standby
0.001	0.98871	0.54005
0.002	0.98552	0.53450
0.003	0.98235	0.52907
0.004	0.97921	0.52376
0.005	0.97610	0.51856
0.006	0.97302	0.51347
0.007	0.96995	0.50848
0.008	0.96692	0.50360
0.009	0.96391	0.49881
0.010	0.96092	0.49412

Table 3: Relation between failure rate λ_p and the Busy Period of the system

	system	
3	Busy period of the system	Busy period of the system
λ_p	with repair and without standby	with repair and standby
0.001	0.42485	0.37431
0.002	0.43562	0.38636
0.003	0.44611	0.39810
0.004	0.45635	0.40954
0.005	0.46634	0.42070
0.006	0.47609	0.43158
0.007	0.48560	0.44218
0.008	0.49488	0.45253
0.009	0.50394	0.46261
0.010	0.51279	0.47246

Table 4: Relation between failure rate λ_p and the profit (with and without standby)

	The profit with	The profit with repair
λ_p	repair and standby	and without standby
0.001	946.23	502.62
0.002	941.96	495.86
0.003	937.74	489.26
0.004	933.58	482.81
0.005	929.47	476.49
0.006	925.41	470.31
0.007	921.39	464.26
0.008	917.43	458.35
0.009	913.52	452.55
0.01	909.64	446.87



Fig. 2: Relation between the failure rate λ_p and the MTSF



Fig. 3: Relation between the failure rate λ_p and the steady state availability

- Figure 3 show relation between the failure rate λ_p and steady state availability
- Figure 4 show relation between the failure rate λ_p and busy period
- Figure 5 show relation between the failure rate λ_p and expected total profit



Fig. 4: Relation between the failure rate λ_p and the busy period



Fig. 5: Relation between the failure rate λ_p and the expected total profit

- Table 4 show relation between failure rate λ_p and expected total profit of the system (with repair and standby and with repair and without standby)
- Figure 2 show relation between the failure rate λ_p and MTSF

DISCUSSION

By comparing the MTTF with respect to failure rate λ_p . theoretically and graphically. It was observing that: The increase of failure rate λ_p at constant $\lambda_c = 0.003$, $\lambda_\beta = 0.007$, $\lambda_4 = 0.01$, $\lambda_3 = 0.03$, $\mu_1 = 0.1$, $\mu_2 = 0.2$, $\mu_3 = 0.3$, $\mu_4 = 0.4$, R =1000, C = 100, the MTTF of the system decreases for both systems with repair and standby and with repair and without standby and without repair and standby. We conclude that: the MTTF of the system with repair and standby is longer than the system without repair and standby, i.e., the system with repair and standby is better than the system without repair and standby.

By comparing the busy period with respect to failure rate λ_p theoretically and graphically. It was observing that: The increase of failure rate λ_p at constant $\lambda_c = 0.003$, $\lambda_\beta = 0.007$, $\lambda_4 = 0.01$, $\lambda_3 = 0.03$, $\mu_1 = 0.1$, $\mu_2 = 0.2$, $\mu_3 = 0.3$, $\mu_4 = 0.4$, R =1000, C= 100, busy period increases for both systems with repair and standby and with repair and without standby. We

conclude that: the busy period of the system with repair and standby is greater than the system with repair and without standby.

Also, by comparing the steady state availability and the profit with respect to failure rate λ_p theoretically and graphically. It was observing that: The increase of failure rate (λ_p), at constant, $\lambda_c = 0.003$, $\lambda_\beta = 0.007$, $\lambda_4 = 0.01$, $\lambda_3 = 0.03$, $\mu_1 = 0.1$, $\mu_2 = 0.2$, $\mu_3 = 0.3$, $\mu_4 = 0.4$, R =1000, C = 100, the steady state availability and the profit function of the system decreases for both systems with repair and standby and with repair and without standby.

CONCLUSION

We conclude also that: the steady state availability and the profit of the system with repair and standby is greater than the system with repair and without standby. i.e., the system with repair and standby is better than the system with repair and without standby.

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